Disc Monopole Antenna with Ring Patches and Meandered Feeder for Radio Frequency Energy Harvesting

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Abstract In this paper, a new wideband antenna with meandered feed line is presented which can be used in radio frequency (RF) energy harvesting. The proposed antenna is designed on 36 by 56.5 mm² FR4 board with thickness of 1.6 mm and dielectric permittivity constant and tangent loss of 4.3 and 0.025, respectively. It consists of circular disc antenna, two ring patches and three rectangular slots on the ground plane as well as a meandered feed line. Although any RF signal could be useful from energy harvesting point of view, the proposed antenna shows a wideband frequency range from 1.59 to 6.62 GHz and 7.44 GHz to 8 GHz in reference to -10dB return loss or better for wideband applications.

Keywords: wideband, monopole antenna, meandering


1. Introduction

All the time, there are wireless transmissions of power at different frequencies, and most of the transmitted energy is wasted. Based on this fact, the concept of radio frequency energy harvesting has been introduced. By energy harvesting, any source of energy at a certain level could be harness to be used for recharging a mobile phones battery; operating battery-less devices and many other applications.

Within the last decade, the wireless transmission technique has begun to open, and adopted in many used portable devices. As the usage of these hand held electronic devices is increasing, the demands for longer battery life are also increasing. Available radio frequency (RF) energy in the environment or areas close to transmission sources provides an opportunity to harvest that energy using frequencies up to ultra wide band (UWB) [1, 2].

There has been research on UWB, which extends from 3.1 GHz to 10.6 GHz according to Federal Communication Commission (FCC), especially for wireless communications [3].

Research on wide bands to cover lower frequencies in the Megahertz range to high frequencies in the Gigahertz range is continuously being carried out [4, 5]. The size of the antenna, which is very important element in wireless application, is different depends on the targeted wideband. It is small for high frequency band and large for low frequency band [6].

The proposed antenna is designed to be used in RF energy harvesting to cover several used bands such as, GSM 1800, GSM 1900, WLAN-2.4, and WLAN-5.2, or any other standard bands.

The proposed antenna is based on a circular disc monopole antenna because of its radiating patch shape to obtain small size; simple structure and wide bandwidth [7].

The proposed antenna uses a combination of different techniques such as creating new paths to current by adding two ring patches on the sides and adding slots on both the radiating and ground planes to increase the bandwidth by making irregular surface currents [8]; cutting a step in upper half of the radiating patch [9] and meandering the feeding line to lengthen the path of the current [10].

Using all these techniques will give additional features to the proposed antenna.

In this paper, two antennas are designed and simulated, using Computer Simulation Technology (CST) Microwave Studio package, to be used for wireless energy harvesting application. The first proposed antenna is a disc monopole with straight feed line (DMSFL), and the second proposed antenna is a disc monopole with meandered feed line (DMMFL).

Both antennas are designed on $W = 36$ mm by $L = 56.5$ mm FR4 substrate with thickness of 1.6 mm and relative dielectric constant of 4.3.

2. DMSFL Antenna Design

The DMSFL antenna is a disc monopole with ring patches and straight feed line. The radiating patch of this antenna is shown in Figure 1.
Figure 1. The radiating patch of DMSFL antenna

All parameters shown in Figure 1 are optimized for better return loss and wider bandwidth. It consists of a disc patch of radius $R = 10.5 \text{ mm}$; two ring patches of outer radius $R_1 = 8.2 \text{ mm}$ and inner radius $R_2 = 6.8 \text{ mm}$; a straight feed line of dimensions $W_f = 3 \text{ mm}$ and $L_f = 31.5 \text{ mm}$; a rectangular slot of size $W_s = 1 \text{ mm}$ by $L_s = 24 \text{ mm}$ and a circular slot of radius $R_m = 1.8 \text{ mm}$ to improve the matching at low frequencies; and additional two circular patches on the top of the rings with radius $R_t = 2.7 \text{ mm}$ are added.

The ground patch of DMSFL antenna is shown in Figure 2.

Figure 2. The ground patch of DMSFL antenna

Again all parameters shown in Figure 2 are optimized for better RL and wider bandwidth. The ground patch is found to be of size $W_g = 34 \text{ mm}$ by $L_g = 30.5 \text{ mm}$ which has two symmetric slots, each is a combination of a circular sector of radius $R_{gs} = 3 \text{ mm}$ and a rectangle of dimensions $W_{gs} = 4 \text{ mm}$ by $L_{gs} = 6 \text{ mm}$. In addition, a third rectangular slot of dimensions $W_{gc} = 3.2 \text{ mm}$ by $L_{gc} = 6 \text{ mm}$ is extracted from the upper edge of the ground patch for better performance.

3. DMSFL Antenna Results and Discussion

The DMSFL antenna is simulated using CST Microwave Studio. The simulated return loss (RL) is shown in Figure 3.

Assuming -10dB return loss level as an acceptable RL, corresponding to a voltage standing wave ratio (VSWR) of 2, Figure 3 shows an interesting band of frequencies starting from 1.71 to 6.11 GHz.

Figure 3. The simulated return loss of DMSFL antenna

The impedance of DMSFL antenna is simulated and the result is shown in Figure 4.

Figure 4. The real and imaginary parts of the $Z$ matrix of DMSFL antenna

It could be noted from Figure 4 that the real part of DMSFL antenna impedance is varying between 50±10 $\Omega$ in the frequency range from 1.71 to 6.11 GHz and the imaginary part is varying between 0 ± 10 $\Omega$ in the same frequency range indicating an acceptable matching with 50$\Omega$.

4. DMMFL Antenna Design

The DMMFL antenna is a disc monopole with ring patches with meandered feed line, as shown in Figure 5, to lengthen the current path of the feeder for better performance.

Figure 5. The radiating patch of DMMFL antenna

All parameters shown in Figure 5 for the radiating patch are fixed to the same optimized values as those of DMSFL antenna except the feed line which is meandered by curved paths successively through all the line with radius of radius of $R_f = 4 \text{ mm}$.

The ground patch of DMMFL antenna is the same as that of DMSFL antenna shown in Figure 2 except the
dimension of \( L_{gs} \) which is optimized to a value of 8 mm as shown in Figure 6.

![Figure 6. The ground patch of DMSFL antenna](image1)

5. DMMFL Antenna Results and Discussion

The DMMFL antenna is simulated using CST Microwave Studio. The simulated return loss (RL) is shown in Figure 7. It shows two interesting bands of frequencies starting from 1.59 to 6.62GHz and from 7.43GHz to nearly 8GHz at -10 dB RL reference level.

![Figure 7. The simulated return loss of DMMFL antenna](image2)

As can be seen from Figure 3 & Figure 7, there has been improvement in the bandwidth of DMMFL antenna by adding 120 MHz to the lower cutoff frequency of DMSFL antenna, and adding another 51MHz to the upper cutoff frequency limit. Besides that, an additional band of frequencies staring from 7.4GHz to nearly 8GHz in reference to -10dB RL level is obtained.

The impedance of DMMFL antenna is simulated and the result is shown in Figure 8.

![Figure 8. The simulated real and imaginary parts of the Z matrix of DMMFL antenna](image3)

It is clear from Figure 8 that by using meandering technique an inductive behavior at 4.06, 5.4, and 6 GHz where it showed capacitive behavior in the straight technique. At 4.58 GHz, the inductive behavior in the straight feed line becomes capacitive with the meandering feed line.

Because DMMFL antenna shows better performance compared to DMSFL antenna, further investigations are carried out.

The gain of DMMFL antenna is simulated as a function of frequency as shown in Figure 9, which shows a gain above 1.4 dB at frequency above 5GHz and maximum gain of 2.5 dB at 2.4 GHz. The impedance matching between the antenna and the port is shown in Figure 10 using Smith chart, where the antenna impedance becomes closer to the line impedance of 49.95 Ω.

![Figure 9. Realized gain of the proposed DMMFL antenna](image4)

![Figure 10. Smith Chart of the proposed DMMFL antenna](image5)

The value of VSWR reaches maximum of 1.755 at 5.25 GHz and doesn’t exceed 2 through the bandwidth as shown in Figure 11.

![Figure 11. Simulated VSWR of DMMFL antenna](image6)
Figure 12 shows the efficiency of the DMMFL antenna. It can be seen that a maximum efficiency of 91.56% at 1.8 GHz and as the frequency increases the efficiency decreases reaching 72.31% at 5.2 GHz.

The current density distribution for the proposed DMMFL antenna at three different frequencies of 1.8, 2.4 and 5.2 GHz are shown in Figure 13. These frequencies are chosen because they present the most common used standards in wireless communication.

The blue, green, and red colors shown in Figure 13 denote low, moderate, and high current density respectively. The electric currents are concentrated along the feeding line, while it is concentrated at the beginning of the patch at 1.8 GHz. On the other hand, the current density is less at 2.4 GHz and starts to spread through the ground patch. At 5.2 GHz, the current is less concentrated at the beginning of the radiating patch and moves to the ring patches of the antenna in asymmetrical manner.

Figure 14 shows the radiation far-field plot in 3D for the two frequencies of 2.4 GHz and 5.2 GHz. Comparing between them, it can be noticed that at 2.4 GHz the radiation is focused around the feed line on both the front and back and less on the sides of the antenna, while at 5.2 GHz the radiation is concentrated around the feed line on one side and the rings of the antenna, which agrees with the current distribution shown in Figure 13.

The blue, green, and red colors shown in Figure 15 denote low, moderate, and high current density respectively. The electric currents are concentrated along the feeding line, while it is concentrated at the beginning of the patch at 1.8 GHz. On the other hand, the current density is less at 2.4 GHz and starts to spread through the ground patch. At 5.2 GHz, the current is less concentrated at the beginning of the radiating patch and moves to the ring patches of the antenna in asymmetrical manner.
Figure 15 shows the simulated E-plane and H-plane at 1.8, 2.4, and 5.2 GHz. It can be noticed that the radiation pattern is nearly Omni-directional as frequency increases.

The size, bandwidth, and gain of the proposed disc monopole with ring patches and meandered feed line (DMMFL) antenna are compared with those given in [6] and [8] as given in Table 1.

| Table 1. Comparison Between DMMFL Antenna with Those in [6] and [8] |
|---|---|---|---|
| Size | Bandwidth | Gain (dB) | Year |
| Ref. [8] | 30 by 51 mm² | 1.98 to 6.46 GHz | 3 | 2010 |
| Ref. [6] | 120 by 150 mm² | 0.77 to 11.23 GHz | 4.3 | 2012 |
| DMMFL | 36 by 56.5 mm² | 1.59 to 6.62 GHz | 2.565 | This paper |

As can be seen from Table 1, the proposed DMMFL antenna has almost the same area as that in [8] but it has a larger bandwidth and that increment in dimensions is necessary to reach the above lower frequency limit of the bandwidth, unlike [6] where it has an area 8 times larger than that of the proposed antenna to achieve double the bandwidth of our proposed antenna. As for the gain, the DMMFL antenna has a gain of 2.58 dB which is less than that given in [6] and [8].

6. Conclusion

The circular disc monopole antenna with two ring patches fed by meandered feed line is presented in this paper. With the overall adjustment and optimization of the geometrical parameters, the proposed antenna can operate between 1.59 to 6.62 GHz and at 7.44 GHz to 8 GHz for wide band applications. By using different techniques, the antenna shows small size, good matching, and acceptable gain to be integrated in portable devices for radio frequency energy harvesting.

References